

NATIONAL EXAMINATION – MAY 2012
04-GEOL-A6 SOIL MECHANICS

3 HOURS DURATION

NOTES:

1. If doubt exists as to the interpretation of any question, the candidate is urged to submit with the answer paper, a clear statement of any assumptions made.
 2. This is a CLOSED-BOOK exam. Only Casio or Sharp approved model calculators are permitted. **A formula sheet and some charts are attached to this exam.**
 3. Questions have the values shown. The total value is 100.
 4. In the absence of specific parameters required in the formulation and solution of problems, the candidates are expected to exercise sound engineering judgment and to clearly state their assumptions.
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NATIONAL EXAMINATIONS – MAY 2012
04-GEOL-A6 SOIL MECHANICS

1. Soil properties

a. A compacted soil sample fills a 944 cm^3 mould. The dry density of the sample is 2065 kg/m^3 , the moisture content is 5% and the Specific Gravity of the solids is 2.6. Calculate the total mass of the sample in the mould, the void ratio, and the saturation.

(Value 10)

b. The hydraulic conductivity of a soil depends on what?

(value 5)

2. Soil Classification.

Classify the soils of figure Q.2 (Page 4) according to the Unified Soil Classification System. The fines of soil A have a liquid limit of 60% and a plastic limit of 20%, while those of soil B have a liquid limit of 30% and a plastic limit of 20%.

(value 10)

3. In situ Stresses / Consolidation and settlement.

A 4m thick sand fill is placed on a layer of Normally-Consolidated clay to pre-consolidate it, as shown on figure Q.3. The free surface (water table) is located at the top of the clay layer and is expected to stay there.

a. Calculate the time it will take for the 4m fill to settle as much as the full consolidation settlement of a 1m fill. Or in other words, when can we remove 3m of the fill and be left with 1m of fill that will not settle anymore?

(value 15)

b. Clays are very frequently observed to be over-consolidated in the field. What causes the over-consolidation of clays?

(value 10)

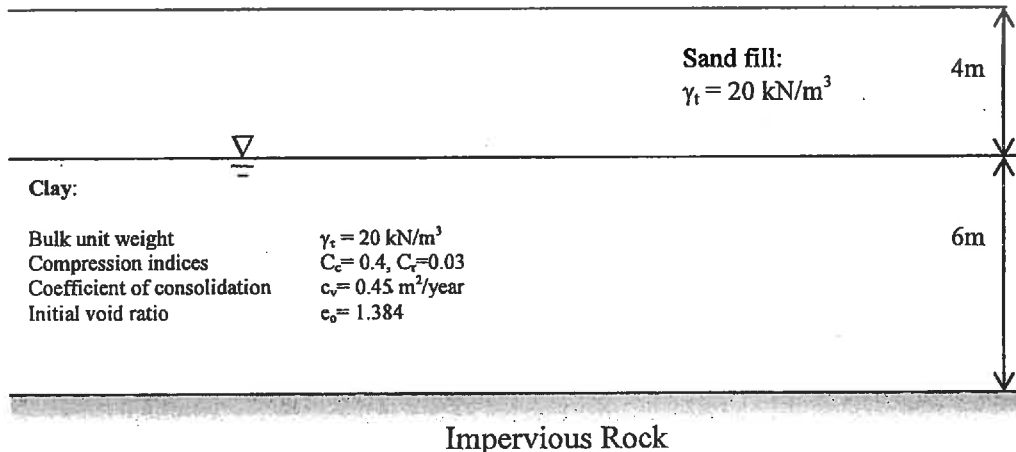


Figure Q.3

NATIONAL EXAMINATIONS – MAY 2012
04-GEOL-A6 SOIL MECHANICS

4. Lateral earth Pressures / Slope Stability

Figure Q.4. shows a Segmental Retaining Wall with geosynthetic reinforcement, installed to stabilize a slope.

- a. Sketch and explain conceptual diagrams of the distribution of forces (no numerical values required) acting on the back of the wall facing and the distribution of forces on the reinforced soil mass. What two theories are most commonly used to calculate the forces on retaining walls?

(value 20)

- b. Sketch and explain two unlikely slope failure surfaces and two more likely ones.

(value 10)

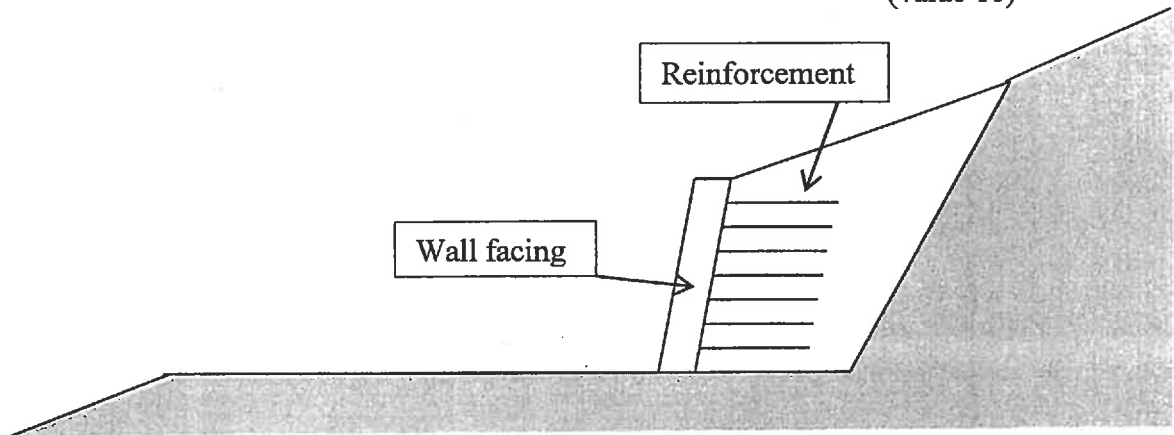


Figure Q.4.

5. Seepage / Groundwater

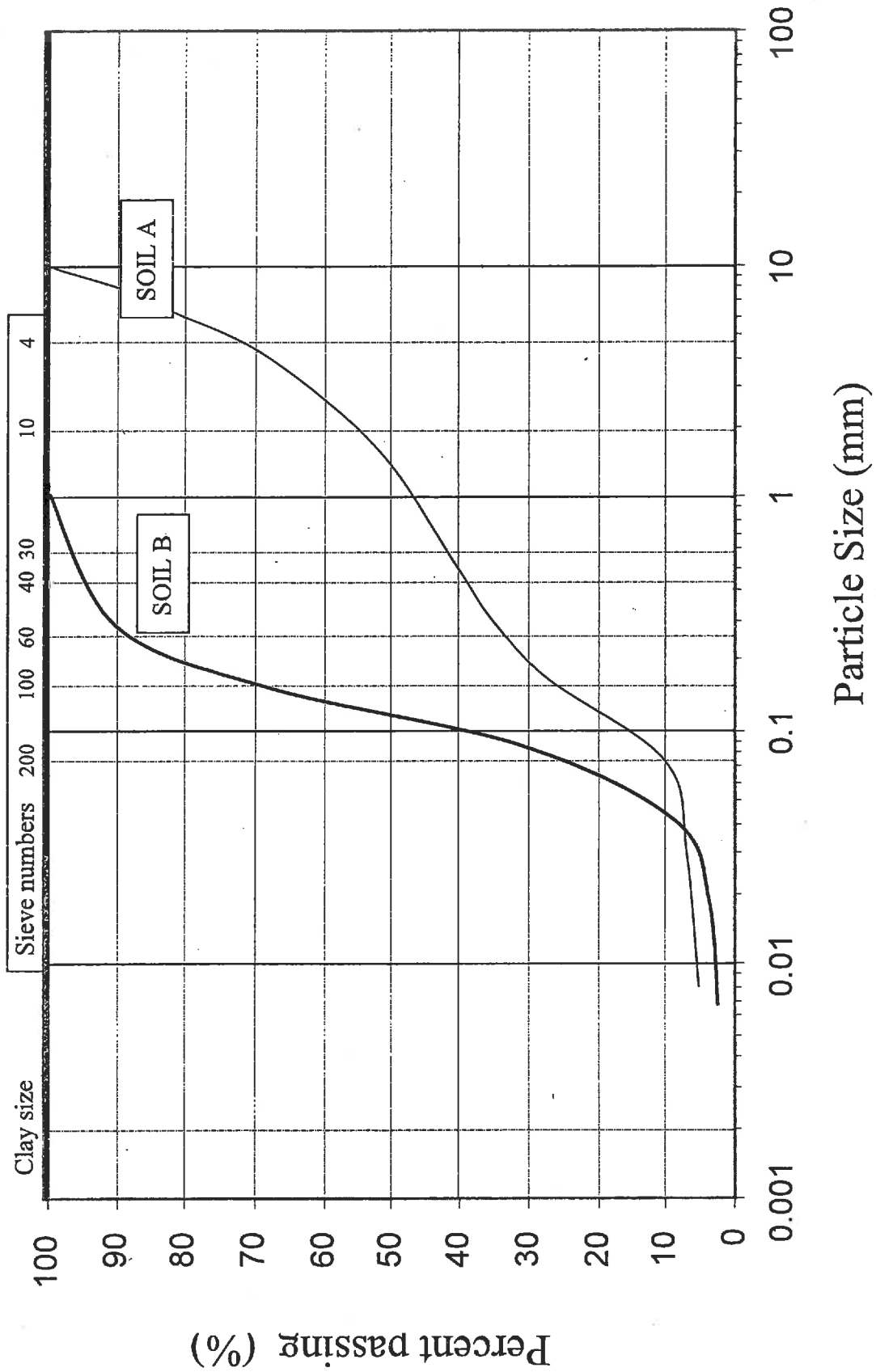
- a. Describe and explain any one potential benefit and any one potential detriment of lowering the water table.

(Value 10)

- b. At the foot of an earth dam, two piezometers were installed one above the other, to record the pore pressure to monitor for potential instabilities. The lower piezometer has an intake at an elevation of 200m above sea level and the upper piezometer has an intake at 205m. The pore water pressure measured at the lower piezometer is 350kPa and the pressure at the upper one is 280kPa. With supporting calculations and assumptions, evaluate the risk of boiling at that location.

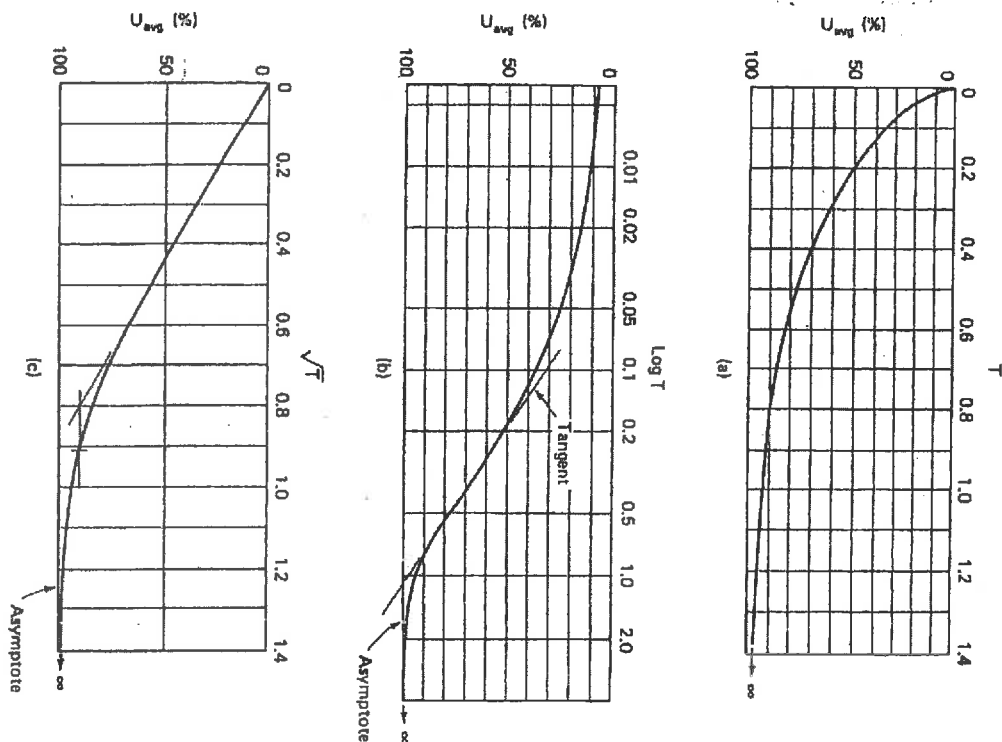
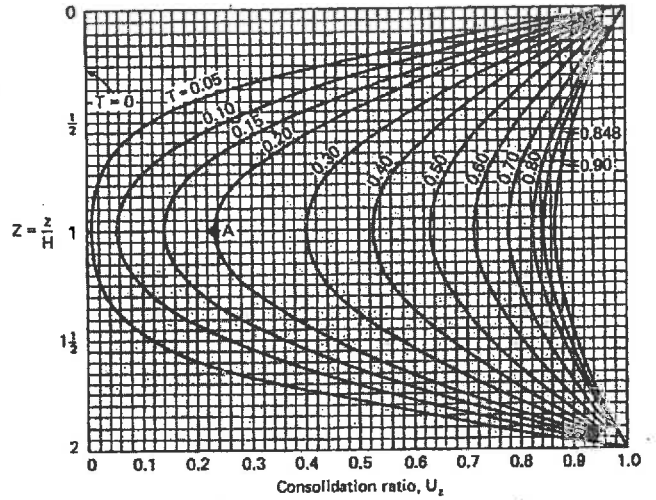
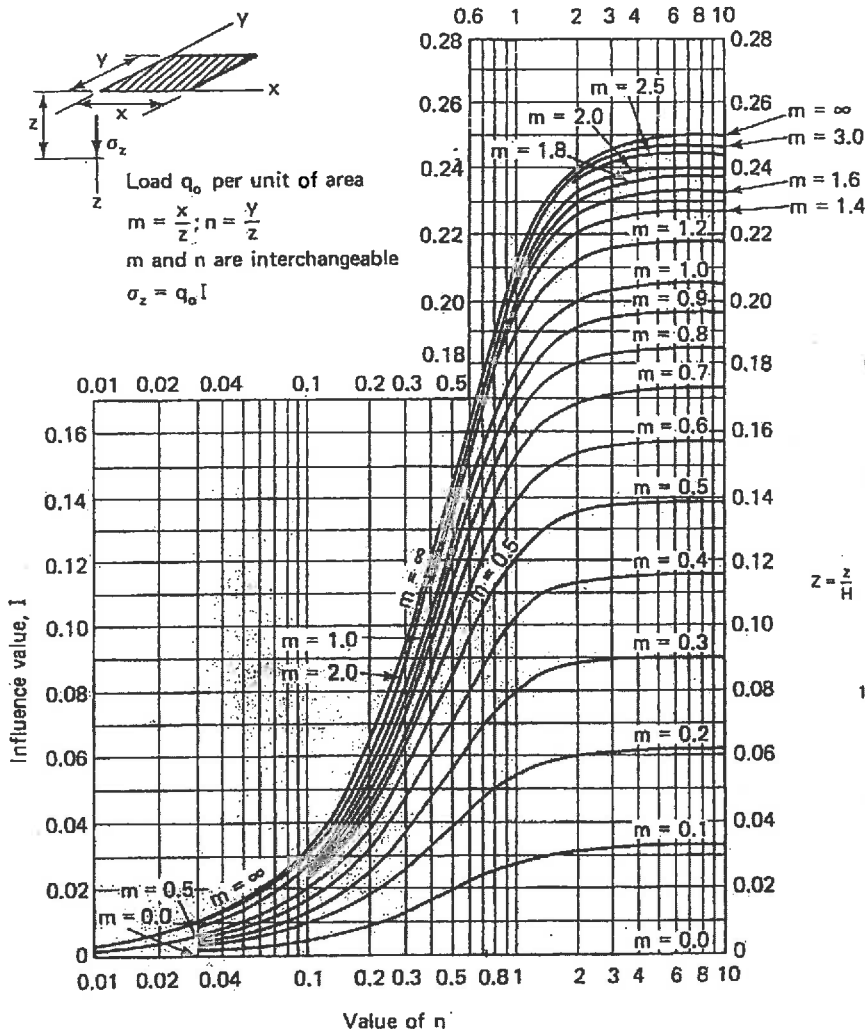
(Value 10)

NATIONAL EXAMINATIONS – MAY 2012
04-GEOL-A6 SOIL MECHANICS



NATIONAL EXAMS – MAY 2012
04-GEOL-A6 SOIL MECHANICS

Formulas and Charts



NATIONAL EXAMS – MAY 2012
04-GEOL-A6 SOIL MECHANICS
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6 of 7

$$\Delta u = B[\Delta\sigma_3 + A(\Delta\sigma_1 - \Delta\sigma_3)]$$

$$\sigma' = \sigma - u$$

$$\tau_f = c' + \sigma' \tan \phi'$$

$$S_c = C_r \left(\frac{H_o}{1+e_o} \right) \log \frac{\sigma'_p}{\sigma'_{vo}} + C_c \left(\frac{H_o}{1+e_o} \right) \log \frac{\sigma'_{vf}}{\sigma'_p}$$

$$T = \frac{c_v t}{H_{dr}^2}$$

$$q = k \Delta h \frac{N_f}{N_d}$$

$$h_t = h_p + z = \frac{u}{\gamma_w} + z$$

$$C_u = \frac{D_{60}}{D_{10}}$$

$$C_c = \frac{(D_{30})^2}{D_{10} D_{60}}$$

$$i = \frac{\Delta h}{l}$$

$$\rho_d = \frac{\rho_t}{(1+w)}$$

$$\psi' = \arctan(\sin \phi') \quad a = c' \cos \phi'$$

$$e = V_v / V_s \text{ (void ratio)}$$

$$n = V_v / V_t \text{ (porosity)}$$

$$w = M_w / M_s \text{ (moisture content)}$$

$$S = V_w / V_v \text{ (saturation)}$$

$$p = \frac{\sigma_1 + \sigma_3}{2}$$

$$q = \frac{\sigma_1 - \sigma_3}{2}$$

$$k_N = \frac{H}{\left(\frac{H_1}{k_1} + \frac{H_2}{k_2} + \frac{H_3}{k_3} \right)}$$

$$k_p = \frac{k_1 H_1 + k_2 H_2 + k_3 H_3}{H}$$

$$k = C D_{10}^2 \quad (C=100, k = \text{cm/s} \ \& \ D_{10} = \text{cm})$$

$$\rho' = \rho_{\text{sat}} - \rho_w \quad \rho_w = 1000 \text{ kg/m}^3$$

$$\gamma_w = 9.81 \text{ kN/m}^3$$

Force → Newton (N) → 1 N = 1 kg m/s²

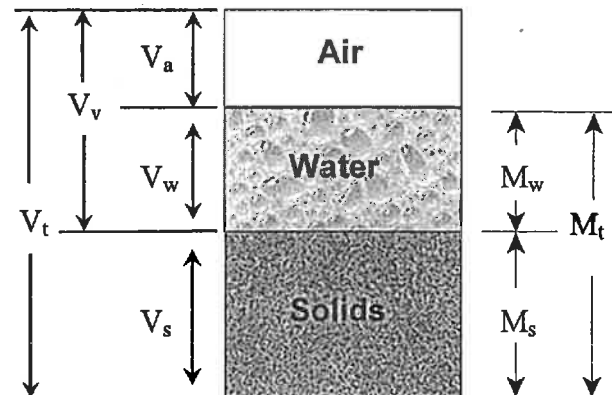
Pressure → Pascal (Pa) → 1 Pa = 1 N/m²
 → 1 kPa = 1 kN/m²

$$N_{\text{corr}} = 100 \times (N - N_{\text{fines}}) / (100 - N_{\text{fines}})$$

$$\Delta\sigma_{v(\text{avg})} = \frac{(\Delta\sigma_{v(\text{top})} + 4\Delta\sigma_{v(\text{mid})} + \Delta\sigma_{v(\text{bot})})}{6}$$

$$K_a = \frac{1 - \sin \phi'}{1 + \sin \phi'} \quad K_p = 1/K_a \quad K_o \approx 1 - \sin \phi'$$

$$\sigma'_h = \sigma'_v K_a - 2C' \sqrt{K_a} \quad \sigma'_h = \sigma'_v K_p + 2C' \sqrt{K_p}$$



NATIONAL EXAMS – MAY 2012
04-GEOL-A6 SOIL MECHANICS

Formulas and Charts

Major Divisions		Group Symbols (†)	Typical Names	Laboratory Classification Criteria
1	Coarse-grained Soils More than half of material is larger than No. 200 (†) (75 µm) sieve size.	3	4 Well-graded gravels, gravel sand mixtures, little or no fines. Poorly graded gravels, gravel-sand mixtures, little or no fines. Silty gravels, gravel-sand-silt mixtures. Clayey gravels, gravel-sand-clay mixtures. Well-graded sands, gravelly sands, little or no fines. Poorly graded sands, gravelly sands, little or no fines. Silty sands, sand-silt mixtures. Clayey sands, sand-clay mixtures.	$C_u = \frac{D_{60}}{D_{10}}$ greater than 4 $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ between 1 and 3 (See Sec. 2-5) Not meeting all gradation requirements for GW Atterberg limits below A-line, or PI less than 4 Atterberg limits above A-line with PI greater than 7 cases requiring use of dual symbols. $C_u = \frac{D_{50}}{D_{10}}$ greater than 6 $C_z = \frac{(D_{30})^2}{D_{10} \times D_{50}}$ between 1 and 3 (See Sec. 2.5) Not meeting all gradation requirements for SW Limits plotting in hatched zone with PI between 4 and 7 are bordering cases requiring use of dual symbols.
2	Sands More than half of coarse fraction is larger than (4.75 mm) sieve size. (For visual classification, 5 mm may be used as equivalent to the No. 4 sieve size) Gravels with fines (appreciable amount of fines) Gravels with little or no fines. Sands with appreciable amount of fines Sands with little or no fines.	GW GP GM GC SW SP SM SC	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity. Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays. Organic silts and organic silty clays of low plasticity. Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts. Inorganic clays of high plasticity, fat clays. Organic clays of medium to high plasticity, organic silts.	Determine percentages of gravel and sand from grain size curves. Depending on percentage of fines (fraction smaller than No. 200 sieve size) coarse-grained soils are classified as follows: Less than 5%: GM, GP, SW, SP More than 12%: GM, GC, SM, SC Borderline cases requiring use of dual symbols.
3	Highly Organic Soils More than half of material is smaller than No. 200 (75 µm) sieve size. The No. 200 sieve size is about the smallest particle visible to the naked eye.	Pt	Peat and other highly organic soils.	Use grain size curve in identifying the fractions as given under field identification. Plasticity Chart For laboratory classification of fine-grained soils

† Boundary classifications: soils possessing characteristics of two groups are designated by combinations of group symbols. For example: GW-GC.
 well-graded gravel sand mixture with clay binder.

‡ All sieve sizes on this chart are U.S. Standard.