

NATIONAL EXAMINATIONS MAY 2016

98-Mar-A1 Applied Thermodynamics and Heat Transfer

3 Hours Duration

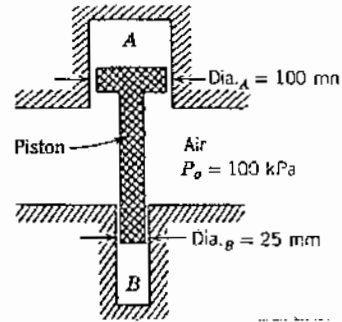
Notes :

1. If doubt exists concerning the interpretation of any question, the candidate is urged to make assumptions and clearly explain what has been assumed along with the answer to the question.
2. The examination is open book. As a consequence, candidates are permitted to make use of any textbooks, references or notes.
3. Any non-communicating calculator is permitted. However, candidates must indicate the type of calculator(s) that they have used by writing the name and model designation of the calculator(s) on the inside of the cover of the first examination book.
4. It is expected that each candidate will have copies of both a thermodynamics text and a heat transfer text in order to make use of the information presented in the tables and graphs contained.
5. The answers to five questions, either three questions from Part A and two questions from Part B or two questions from Part A and three questions from Part B, comprise a complete examination.
6. Candidates must indicate the answers that they wish to have graded on the cover of the first examination book. Otherwise the answers will be graded in the order in which they appear in the examination book(s) up to a maximum of three answers per section.
7. The answer to any question carries the same value in the grading.

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PART A - THERMODYNAMICS

1.(a) Gas is contained in two cylinders A and B connected by a piston having two different diameters as depicted in the illustration. The mass of the piston is 10 kg and the gas pressure inside cylinder A is 200 kPa. Determine the gas pressure inside cylinder B.



(b) Saturated water vapour at 200°C is contained in a cylinder fitted with a piston. The initial volume of the steam is 0.01 m^3 . The steam expands in a quasiequilibrium isothermal process until the final pressure is 200 kPa and in so doing does work against the piston. How much work is done during the process? How much error would be made by assuming the steam to behave as an ideal gas?

2. A combined reheat / regeneration cycle utilizes steam as the working fluid. The steam enters the high pressure turbine at 3.5 MPa and 350°C from which some is extracted at 0.8 MPa for the purposes of feedwater heating. The remainder of the steam is reheated to 350°C after which it enters the low pressure turbine from which some is extracted at 0.2 MPa for feedwater heating. The condenser pressure is 10 kPa and both feedwater heaters are open. Depict the cycle on a T-s diagram and determine the thermal efficiency and the net work output per kilogram of flowing steam.

3. Air enters the compressor of a Brayton cycle at 20°C and 100 kPa and leaves at a pressure of 475 kPa. The maximum temperature of the cycle is limited to 870°C by metallurgical considerations. Assuming a compressor efficiency of 82%, a turbine efficiency of 85% and a pressure drop of 13.7 kPa between the compressor and the turbine, determine (a) the pressure and temperature at each point in the cycle (b) the net work of the cycle (c) the thermal efficiency of the cycle and the percentage of the turbine work required to drive the compressor. Sketch the cycle on a temperature entropy diagram.

4. The following test data were obtained with a Freon-12 vapour compression refrigeration system operating at steady state.

Condenser pressure	700 kPa	
Evaporator pressure	150 kPa	
Temperature at compressor inlet		0°C
compressor outlet		70°C
condenser inlet		60°C
condenser outlet		15°C
expansion valve inlet		20°C
evaporator outlet		-10°C

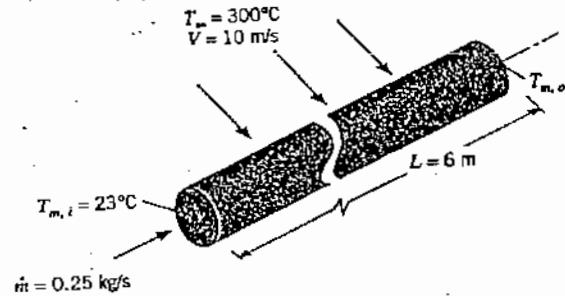
The heat transferred from the refrigerant during compression is 3.35 kJ/kg. Depict the refrigeration cycle on a T-s diagram and determine the coefficient of performance of the cycle and the thermal efficiency of the compression process.

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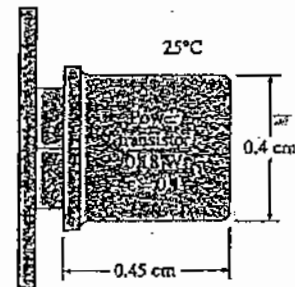
PART B - HEAT TRANSFER

5. Steam flows through a copper tube having an outside diameter $D = 2.54$ cm and a wall thickness $\delta = 0.54$ cm. The inside surface temperature $T_i = 100^\circ\text{C}$ and the temperature of the room in which the tube is located $T_\infty = 27^\circ\text{C}$. Determine the thickness of insulation having thermal conductivity $k = 0.0875$ W/m $^\circ\text{C}$ required to reduce the heat loss to the surrounding air by 95% when the tube is cooled by forced convection heat transfer where $\bar{h} = 55$ W/m 2 $^\circ\text{C}$. What would the outside surface temperature T_o be under these conditions ?

6. Oil flowing at $\dot{m} = 0.25$ kg/s enters a thin-walled tube 50 mm diameter by 6 m long at $T_{m,i} = 23^\circ\text{C}$ where it is heated by a hot gas at $T_\infty = 300^\circ\text{C}$ moving in crossflow over the tube at $V = 10$ m/s. The gas may be assumed to have the same thermophysical properties as those of air. In order to prevent the oil overheating and decomposing, the temperature of the wall must not exceed $T_c = 100^\circ\text{C}$ anywhere along the tube. Will there be any problem associated with heating the oil under these conditions ?



7. The illustration depicts a power transistor that dissipates 0.18 W when the temperature of the enclosure in which it is located is 35°C and the temperature of the air surrounding it is 25°C . The emissivity of its surface is 0.1. Disregarding any heat transfer from the base, determine the surface temperature of the power transistor.



8. A crossflow heat exchanger is comprised of 40 thin-walled tubes 1 cm in diameter located in a duct 1 m x 1 m in cross section. Cold water ($C_p = 4180$ J/kg $^\circ\text{C}$) enters the tubes at 18°C with an average velocity of 3 m/s while hot air ($C_p = 1010$ J/kg $^\circ\text{C}$) enters the channel at 130°C and 105 kPa with an average velocity of 12 m/s. If the overall heat transfer coefficient is 80 W/m 2 $^\circ\text{C}$, determine the temperatures at which the water and the air leave the heat exchanger and the rate of heat transfer.

The End

Thermodynamic Properties of Freon-12 (Dichlorodifluoromethane)^a

Saturated Freon-12

Temp. °C	Abs. Press. MPa P	Specific Volume m ³ /kg			Enthalpy kJ/kg			Entropy kJ/kg K		
		Sat. Liquid <i>v_f</i>	Evap. <i>v_g</i>	Sat. Vapor <i>v_g</i>	Sat. Liquid <i>h_f</i>	Evap. <i>h_g</i>	Sat. Vapor <i>h_g</i>	Sat. Liquid <i>s_f</i>	Evap. <i>s_g</i>	Sat. Vapor <i>s_g</i>
-90	0.0028	0.000 608	4.414 937	4.415 545	-43.243	189.618	146.975	-0.2084	1.0352	0.8268
-85	0.0042	0.000 612	3.036 704	3.037 316	-38.968	187.608	148.640	-0.1854	0.9970	0.8116
-80	0.0062	0.000 617	2.137 728	2.138 345	-34.688	185.612	150.924	-0.1630	0.9609	0.7979
-75	0.0088	0.000 622	1.537 030	1.537 651	-30.401	183.625	153.224	-0.1411	0.9266	0.7855
-70	0.0123	0.000 627	1.126 654	1.127 280	-26.103	181.640	155.536	-0.1197	0.8940	0.7744
-65	0.0168	0.000 632	0.840 534	0.841 166	-21.793	179.651	157.857	-0.0987	0.8630	0.7643
-60	0.0226	0.000 637	0.637 274	0.637 910	-17.469	177.653	160.184	-0.0782	0.8334	0.7552
-55	0.0300	0.000 642	0.490 358	0.491 000	-13.129	175.641	162.512	-0.0581	0.8051	0.7470
-50	0.0391	0.000 648	0.382 457	0.383 105	-8.772	173.611	164.840	-0.0384	0.7779	0.7396
-45	0.0504	0.000 654	0.302 029	0.302 682	-4.896	171.558	167.163	-0.0190	0.7519	0.7329
-40	0.0642	0.000 659	0.241 251	0.241 910	-0.000	169.479	169.479	-0.0000	0.7269	0.7269
-35	0.0807	0.000 666	0.194 732	0.195 398	4.416	167.368	171.784	0.0187	0.7027	0.7214
-30	0.1004	0.000 672	0.158 703	0.159 375	8.854	165.222	174.076	0.0371	0.6795	0.7165
-25	0.1237	0.000 679	0.130 487	0.131 166	13.315	163.037	176.352	0.0552	0.6570	0.7121
-20	0.1509	0.000 685	0.108 162	0.108 847	17.800	160.810	178.610	0.0730	0.6352	0.7082
-15	0.1826	0.000 693	0.090 326	0.091 018	22.312	158.534	180.846	0.0906	0.6141	0.7046
-10	0.2191	0.000 700	0.075 946	0.076 646	26.851	156.207	183.058	0.1079	0.5936	0.7014
-5	0.2610	0.000 708	0.064 255	0.064 963	31.420	153.823	185.243	0.1250	0.5736	0.6986
0	0.3086	0.000 716	0.054 673	0.055 389	36.022	151.376	187.397	0.1418	0.5542	0.6960
5	0.3626	0.000 724	0.046 761	0.047 485	40.659	148.859	189.518	0.1585	0.5351	0.6937
10	0.4233	0.000 733	0.040 180	0.040 914	45.337	146.265	191.602	0.1750	0.5165	0.6916
15	0.4914	0.000 743	0.034 671	0.035 413	50.058	143.586	193.644	0.1914	0.4988	0.6897
20	0.5673	0.000 752	0.030 028	0.030 780	54.828	140.812	195.641	0.2076	0.4803	0.6879
25	0.6516	0.000 763	0.026 091	0.026 854	59.653	137.933	197.586	0.2237	0.4626	0.6863
30	0.7449	0.000 774	0.022 734	0.023 508	64.539	134.936	199.475	0.2397	0.4451	0.6848
35	0.8477	0.000 786	0.019 855	0.020 641	69.494	131.805	201.299	0.2557	0.4277	0.6834
40	0.9607	0.000 798	0.017 373	0.018 171	74.527	128.525	203.051	0.2716	0.4104	0.6820
45	1.0843	0.000 811	0.015 220	0.016 032	79.647	125.074	204.722	0.2875	0.3931	0.6806
50	1.2193	0.000 826	0.013 344	0.014 170	84.868	121.450	206.298	0.3034	0.3758	0.6792
55	1.3663	0.000 841	0.011 701	0.012 542	90.201	117.565	207.766	0.3194	0.3582	0.6777
60	1.5259	0.000 858	0.010 253	0.011 111	95.665	113.443	209.109	0.3355	0.3405	0.6760
65	1.6988	0.000 877	0.008 971	0.009 847	101.279	109.024	210.303	0.3518	0.3224	0.6742
70	1.8858	0.000 897	0.007 828	0.008 725	107.067	104.255	211.321	0.3683	0.3038	0.6721
75	2.0874	0.000 920	0.006 802	0.007 723	113.058	99.068	212.126	0.3851	0.2845	0.6697
80	2.3046	0.000 946	0.005 875	0.006 821	119.291	93.373	212.665	0.4023	0.2644	0.6667
85	2.5380	0.000 976	0.005 029	0.006 005	125.818	87.047	212.865	0.4201	0.2430	0.6631
90	2.7885	0.001 012	0.004 246	0.005 258	132.708	79.907	212.614	0.4385	0.2200	0.6585
95	3.0569	0.001 056	0.003 508	0.004 563	140.068	71.658	211.726	0.4579	0.1946	0.6526
100	3.3440	0.001 113	0.002 790	0.003 903	148.076	61.768	209.843	0.4788	0.1655	0.6444
105	3.6509	0.001 197	0.002 045	0.003 242	157.085	49.014	206.099	0.5023	0.1296	0.6319
110	3.9784	0.001 364	0.001 098	0.002 462	168.059	28.425	196.484	0.5322	0.0742	0.6064
112	4.1155	0.001 792	0.000 005	0.001 797	174.920	0.151	175.071	0.5651	0.0004	0.5655

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